

# AN12242

## NxH3670 headphone antenna

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Application note

### Document information

Information	Content
Keywords	NxH3670, headphone antenna
Abstract	This document describes antenna design guidelines and evaluation methods using the NxH3670.



Revision history		
Rev	Date	Description
1.0	20180927	first issue

## 1 Introduction

This application note is intended as a practical guide to design and validate an antenna for a 2.4 GHz headphone application with radio ICs of the NxH3670. The aim is to provide the required understanding to design such an application specific antenna and to achieve the best performance for RF communication at 2.4GHz.

### Notes:

- As a prerequisite, it is assumed that the reader has a basic understanding on how to use a Radio IC of the NxH3670. This application note cannot and does not replace any of the relevant radio IC datasheets.
- As there are many parameters influencing the overall performance, a basic RF knowledge is needed to design an RF antenna.
- Design hints on how to place the components on a PCB are not included.
- All antenna measurements need to be always performed at the final mounting position to consider effects of incorporation into a product.

The guideline covers the following items:

- A detailed description of the antenna structure.
- The antenna performance validation section describes the required tools and measuring setups to determine the antenna parameters obtained with a connected measurement and a radiated measurement in an anechoic room.

### 1.1 Reference documents

- Data sheet NxH3670

### 1.2 Reference simulation tools

- CST Microwave Studio: 3D Electromagnetic Simulation Tool

## 2 Description of the antenna

A circular electronic board that incorporates electronic components and a conductive ground plane form the antenna. The board has a rectangular slot in its ground plane with an open end and a closed end as shown in [Figure 1](#).

The open end is at the edge of the ground plane and the electrical length of the slot is a quarter wavelength of the transmission frequency approximately. The slot is filled with a non-conductive substrate material.

The diameter ( $\Phi$ ) of the circular ground plane equals an electrical length of a halve wavelength of the transmission frequency. In this way, the ground plane acts as an efficient antenna for a relatively large frequency band.

Oval shaped electronic boards can also be used. However, in this document we provide the dimensions for designing a circular conductive board antenna.

The antenna feeding port has two feeding connections, F1 and F2, on opposite sides of the slot near the closed end. One feeding connection is passing the signal from the transceiver to the slot and vice versa. The other connection is providing the connection to ground to allow this unbalanced feeding configuration.

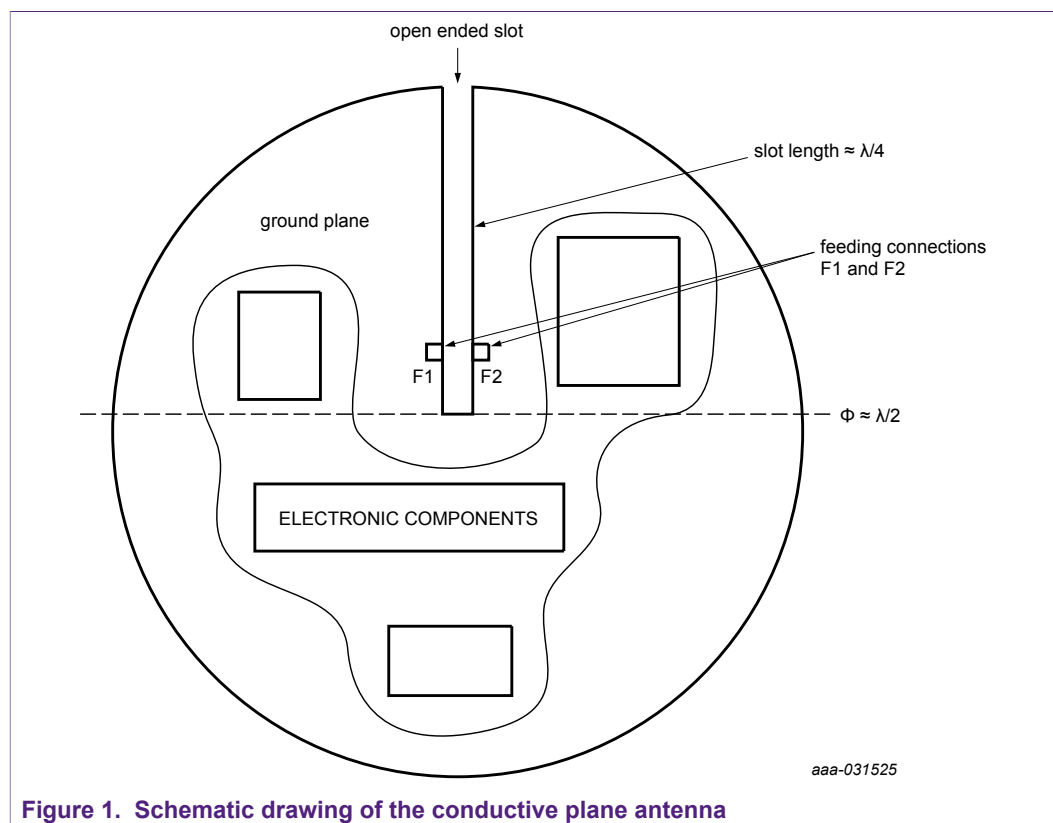


Figure 1. Schematic drawing of the conductive plane antenna

### 2.1 Antenna layout

In what follows, reported values correspond to an antenna design on an FR4 substrate board of approximately 1 mm thickness. When designing the conductive plane antenna for an operation frequency of 2.45 GHz, the circular board is given a diameter of approximately 50 mm. The straight slot is designed with a length of 19.2 mm and a

width of 1 mm. To allow horizontally and vertically polarized antenna radiation, the slot is positioned under an angle of 45 degrees regarding the vertical direction. The radiation pattern is shown in [Section 3.2.2.2](#). The antenna feed point is positioned at a distance of 3.8 mm from the closed end of the slot. [Figure 2](#) clarifies these dimensions.

As the circular board is used to mount electronic components as well, following guidelines must be considered. When more than 2 layers are used in the PCB design, the slot which is copper-free must be repeated as such on all layers. A series of via holes is placed on both sides of the slot with a regular spacing in between them to ensure a good ground connection.

The antenna feeding connection that passes the signal from the balun - connected to the NxH3670 - to the slot is given by the red trace in [Figure 2](#). If necessary, provisions for matching (orange pads) are available to be populated along this trace. The second feeding connection, which is the ground, is implemented by a trace (shown in blue on [Figure 2](#)) on the opposite side of the slot with via holes connecting to the ground plane. See [Figure 3](#) for a more practical implementation.

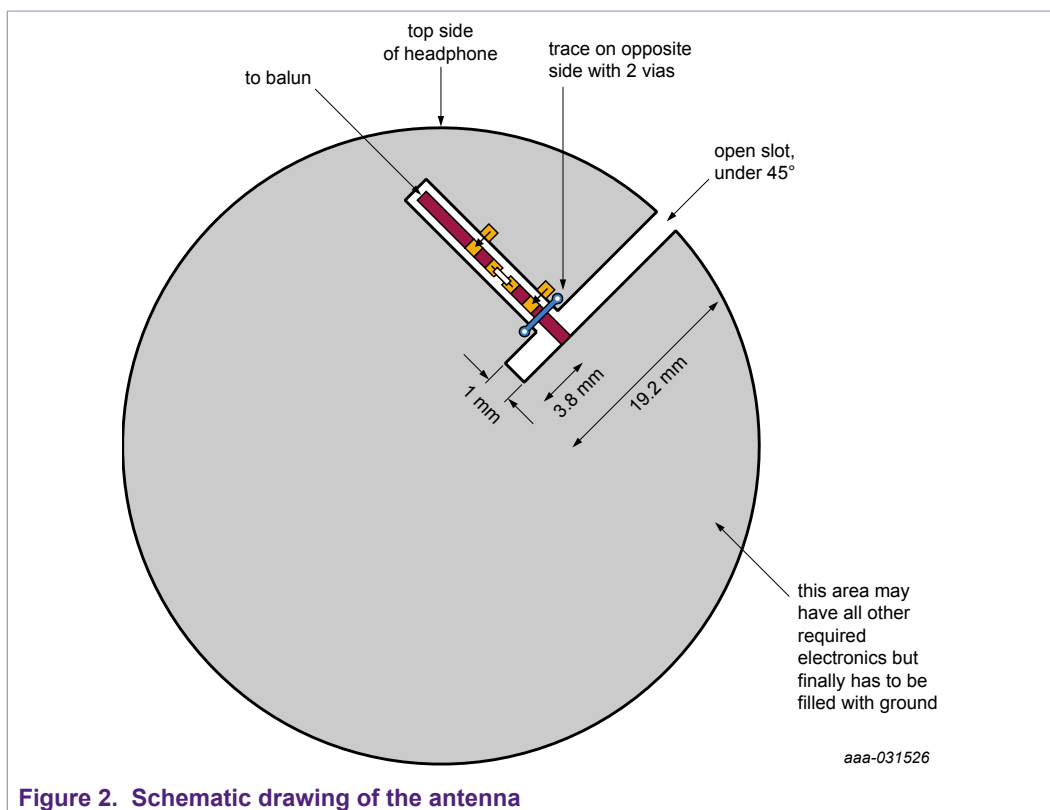


Figure 2. Schematic drawing of the antenna

## 2.1.1 Design guidelines

### 2.1.1.1 Assumptions

Carrier frequency: 2400 MHz to 2480 MHz

Radio IC: NxH3670

### 2.1.1.2 Design targets

Return Loss  $|S_{11}| \leq -10$  dB from 2400 MHz to 2480 MHz

Bandwidth  $\geq 80$  MHz

Maximum gain  $\geq 0$  dBi for the vertical and the horizontal polarization

The antenna must support the vertical polarization and the horizontal polarization.

### 2.1.1.3 Material

- Dielectric material = FR4 1080
- Dielectric constant = 4.2
- Manufacturer: Shenzhen Multilayer PCB Technology Co, Ltd.
- Substrate thickness: 1.1 mm
- Multilayer printed circuit board
- Cu thickness: 17.5  $\mu$ m
- Plated through hole vias at the spiral antenna of 0.4 mm diameter
- via copper thickness: 0.1 mm
- drill size: 0.2 mm

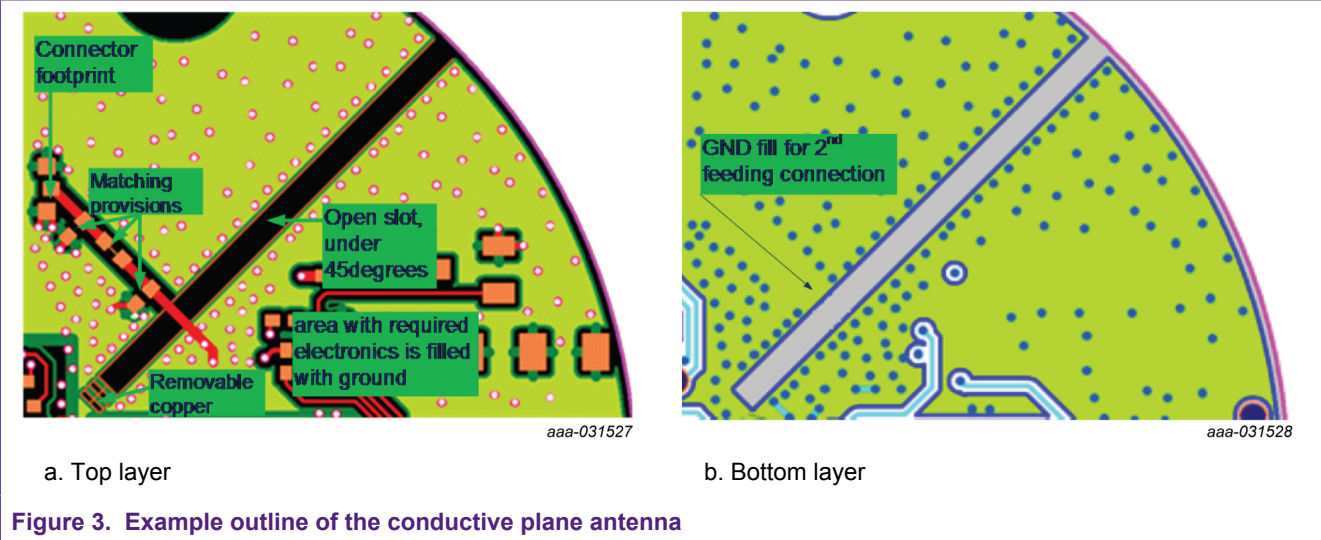
### 2.1.1.4 Planar Outline

In [Figure 3](#), one can find an outline of the conductive plane antenna. The open slot is copper free on all layers and surrounded by numerous via holes on either side connecting the ground to each of the layers.

The red trace on the top layer in [Figure 3](#) shows the antenna feeding connection that passes the signal from the balun to the slot. We have chosen to provide a connector at the left end of this trace (see connector footprint). If necessary, provide this connector in the layout to allow optimizing the matching of the antenna. Provisions to place matching components are foreseen. At the closed end of the slot, provisions are in place, so copper can be scratched off to make the slot longer, if necessary.

The second feeding connection, the ground, is implemented by a copper fill marked by the arrow in the right outline of [Figure 3](#). To ensure a good ground connection, a series of via holes (up to 50 in total) are placed on both sides of the slot and all layers with a regular spacing in between them. These vias are spaced at about 0.3 mm from the slot.

As can be observed, the area surrounding the electronics should be filled with ground. The board diameter is 50 mm and about 0.4 mm clearance area is provided at the edge of the board.



2.1.1.5 Stack up

The reference design is using a multilayer PCB with the following stack up. As mentioned before, the slot which is copper-free must be in place on all layers.

Table 1.

NO.	Stackup			Thickness [mm]
1	GTL		1080 FR-4 1080	0.0175
2	PP			0.15
3	L2T-L3B			0.8
4	PP			0.15
5	GBL			0.0175

### 3 Antenna parameters validation

#### 3.1 Connected measurement

The measurement of the return loss or the  $|S_{11}|$  is done in a connected manner. To retrieve the matching components to provide a 50-ohmic antenna input connection, an UFL connector is soldered at the end of the signal trace connecting to the slot as mentioned earlier.

##### 3.1.1 S-parameter measurement

The return loss or  $|S_{11}|$  measurement of the antenna in air is given in [Figure 5](#) when the matching network available is not populated with L or C reactive matching components. Only a 0  $\Omega$  resistor is connected in series as shown in [Figure 4](#). Attention must be paid to the cable connecting to the UFL connector: the coaxial cable should be kept perpendicular regarding the conductive plane antenna to avoid it from contributing to the radiation of the antenna.

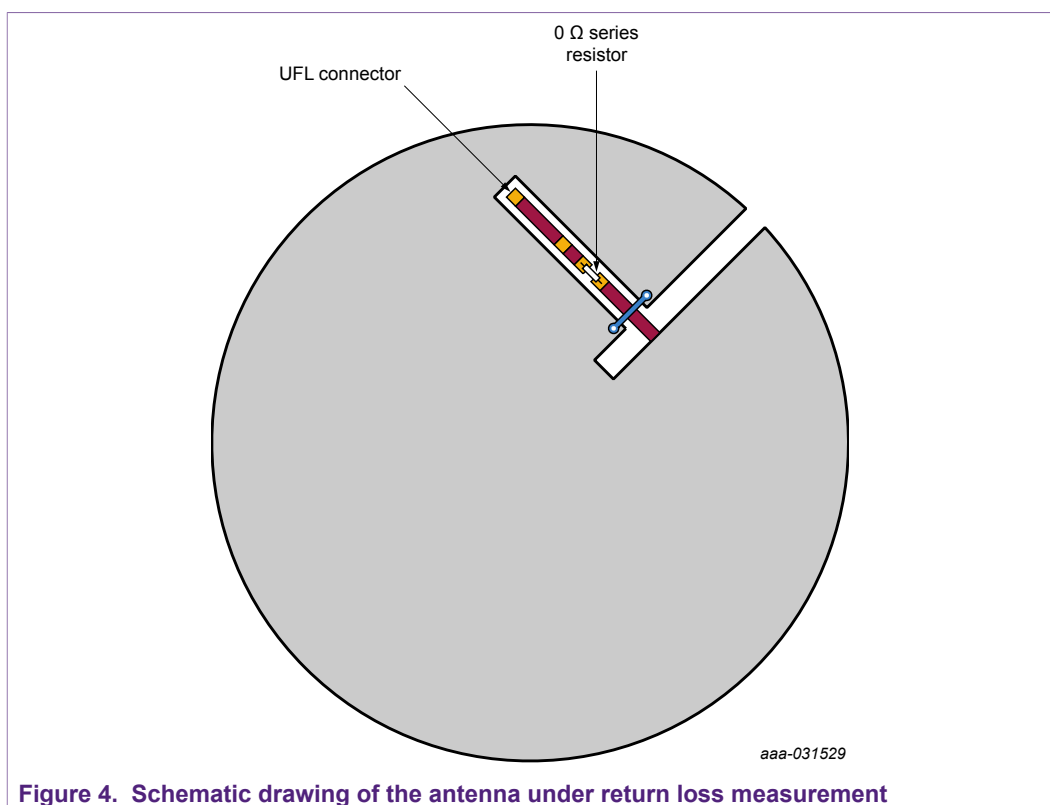
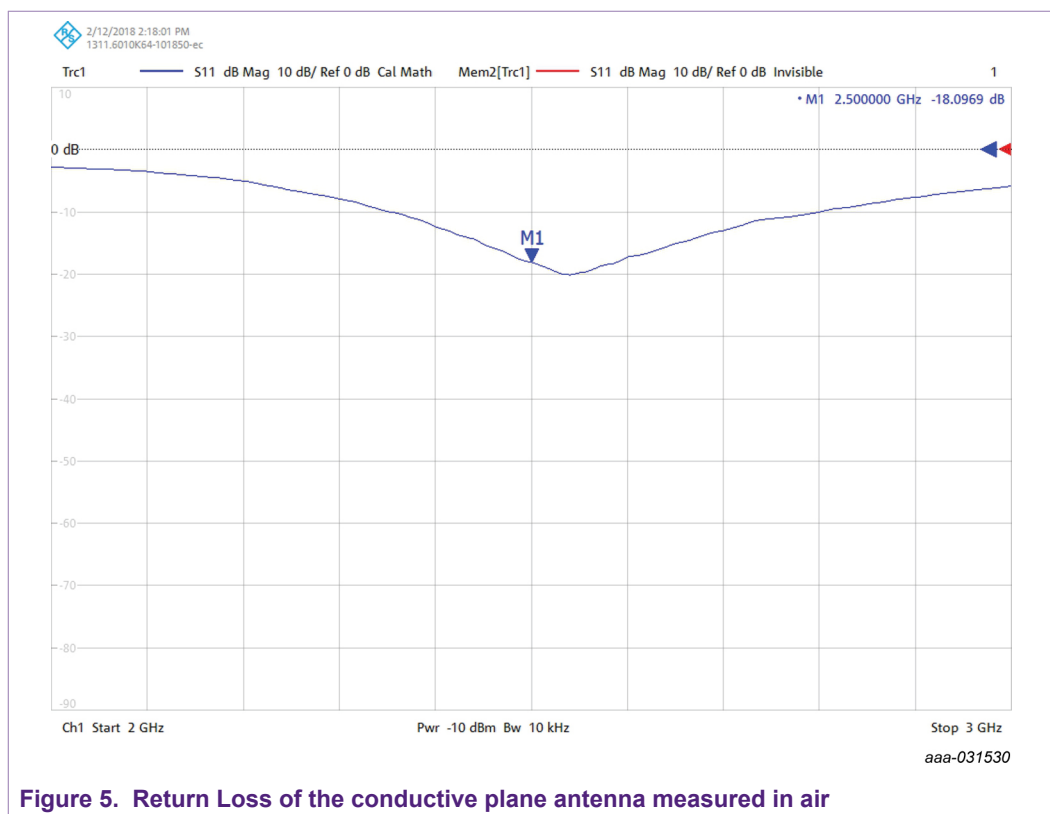


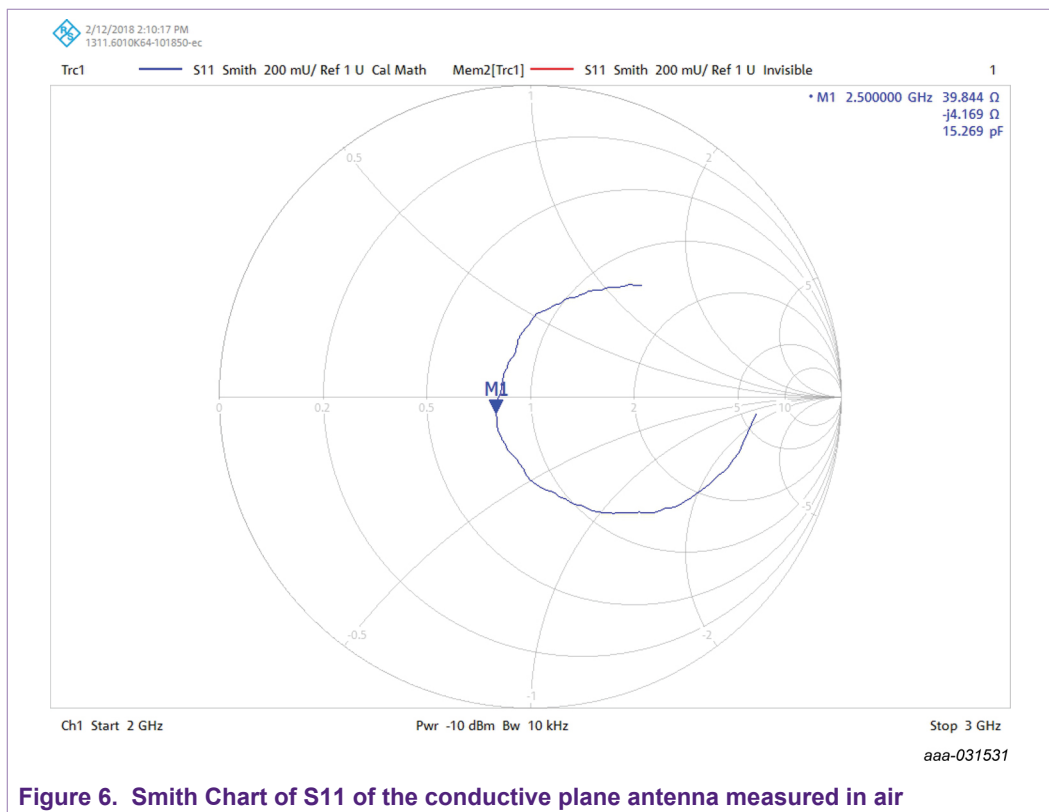
Figure 4. Schematic drawing of the antenna under return loss measurement



**Figure 5. Return Loss of the conductive plane antenna measured in air**

$|S_{11}| < -10$  dB at 2.5 GHz for a bandwidth larger than 300 MHz. Hence, the design target is more than achieved. Mounting the antenna in a headphone, near the head of a user, then maintains a good return loss thanks to the wide bandwidth of the antenna.

The Smith Chart in [Figure 6](#) shows that  $S_{11} = (40 - 4j) \Omega$  at 2.5 GHz.



### 3.2 Radiated measurements

Since the performance of the antenna must be considered when it is integrated in an actual product, we have opted to incorporate the conductive plane antenna inside a fully functional headphone. It is expected that the conductive parts inside the functional headphone and the speaker, which can be 5 cm in diameter, influences the antenna performance.

Hence, the conductive plane antenna is integrated inside the left earpiece of a functional headphone (see [Figure 7](#)). The spacing between the conductive plane antenna and the speaker ( $\Phi = 5$  cm) is chosen to be approximately 6 mm. As speaker and antenna are 5 cm in diameter, they are aligned to cover each other.



aaa-031532

**Figure 7. The conductive plane antenna integrated in a commercially available headphone**

The radiated measurements of the antenna are performed with the headphone on a SAM phantom head (SAM-V4.5BSE by Speag in [Figure 8](#)). A receiving horn antenna captures the vertical and horizontal polarization transmitted by the conductive plane antenna.



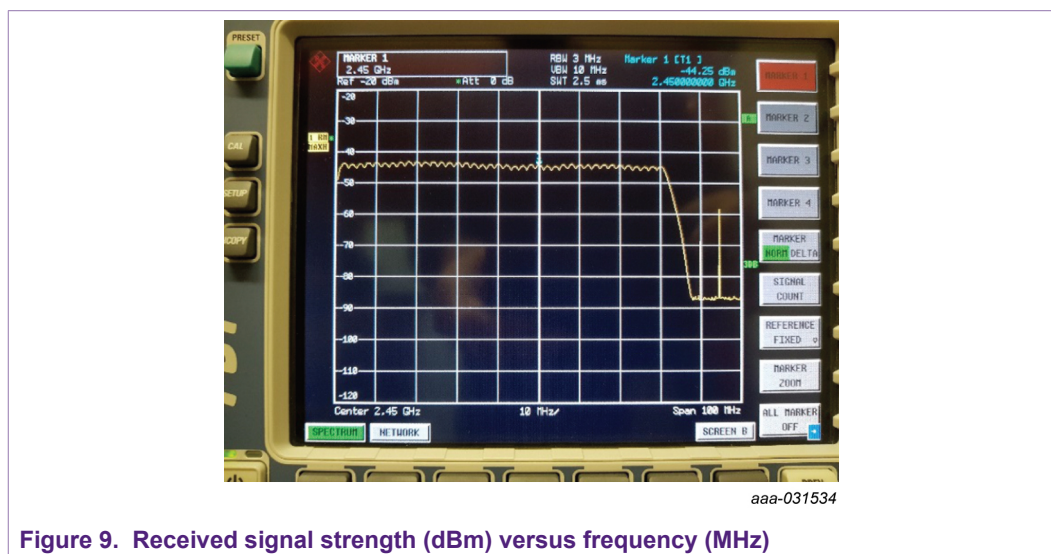
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**Figure 8. Radiated measurements of the antenna inside a headphone on a SAM phantom head mounted in an anechoic room**

### 3.2.1 Radiated antenna bandwidth

Settings of the transceiver:

- Output power: 0 dBm
- Frequency: 2400 MHz to 2480 MHz
- Modulation: off
- Carrier: sweeping
- The antenna supports the required bandwidth from 2400 MHz to 2480 MHz (see [Figure 9](#)).



### 3.2.2 Antenna radiation pattern

#### 3.2.2.1 Conductive plane antenna in functional headphone on a SAM head

The conductive plane antenna is integrated in the left earpiece of the headphone and is then mounted on the left ear of the SAM phantom head. [Figure 10](#) depicts the amount of energy transmitted in the vertical and horizontal polarization by the conductive plane antenna as captured by a receiving horn antenna. The yellow shape in [Figure 10](#) represents the SAM phantom head and the black box represents the earpiece with integrated antenna. Antenna radiation patterns are measured in the horizontal plane.

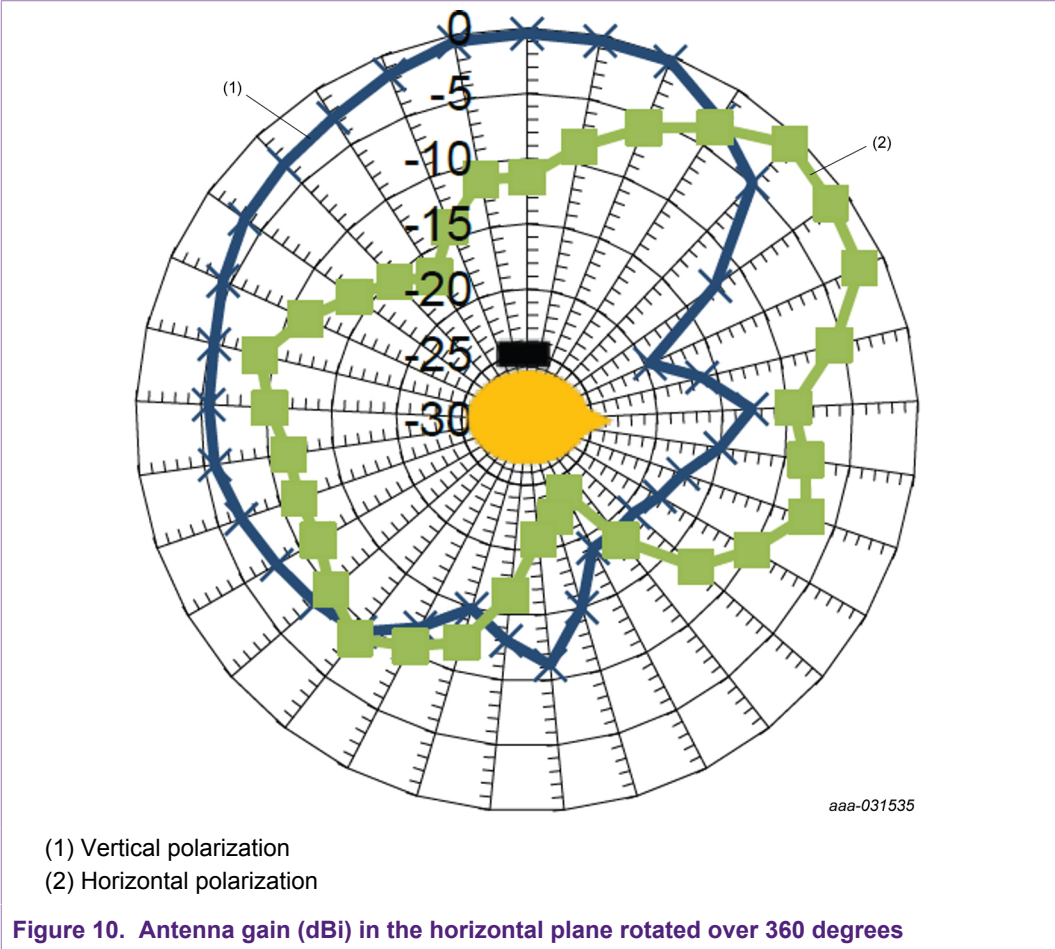
The loss of measuring cables, the horn antenna gain, the path loss in the anechoic room and the input power of the IC are calibrated such that the received signal strength measured by the spectrum analyzer is a measure for the antenna gain in dBi<sup>1</sup> of the conductive plane antenna.

Both polarizations are transmitted and received to a similar extent as can be observed in [Figure 10](#) and in [Table 2](#). The maximum gain is equal in both polarizations and the average gain is the highest in the vertical polarization.

The conductive plane antenna was also measured with the slot positioned vertically and horizontally inside the headphone as opposed to under an angle of 45 degrees. The vertical slot was then yielding dominantly horizontally polarized antenna radiation and the

<sup>1</sup> Antenna gain is here defined as the ratio of the power produced by the antenna to the power produced by a hypothetical lossless isotropic antenna, which is equally sensitive to signals from all directions. This ratio is expressed in "decibels-isotropic" or dBi.

horizontal slot vertically polarized antenna radiation. The property of tilting the slot in the head phone product to achieve either or both polarizations is very beneficial.



With the SAM phantom head in the setup, one would expect to see absorption by the phantom head tissue and hence no energy at the opposite side of the head. However, the conductive parts inside the functional headphone such as the speaker results in additional antenna radiation at the opposite side of the head. The radiation pattern also shows drops in gain due to reflections.

Table 2. Antenna gain (dBi) in the horizontal plane: maximum, minimum and average value over a rotating angle of 360 degrees in the horizontal plane

Gain (dBi)	Vertical polarization	Horizontal polarization
maximum	-0.43	-0.83
minimum	-19.63	-23.73
average	-9.35	-11.13

3.2.2.2 Conductive plane antenna in empty head phone shell on a SAM head

As an illustration, the radiation pattern measured on the conductive plane antenna embedded in an empty head phone without conductive parts is depicted in Figure 11. The purpose is showing that the radiation pattern then does not show energy at the opposite side of the head when there is minimal reflection by the head phone.

The antenna gain is highest perpendicular to the left ear. There is substantially less gain to the back and the front of the user. As can be seen in [Figure 11](#), a severe decrease in performance is found at the other side of the headphone due to absorption by the tissue of the head. As expected, both polarizations are again present in the radiation pattern of the antenna. The energy in the vertical polarization is higher than in the horizontal polarization. The cause can be a slight misalignment when the headphone is on the SAM head.

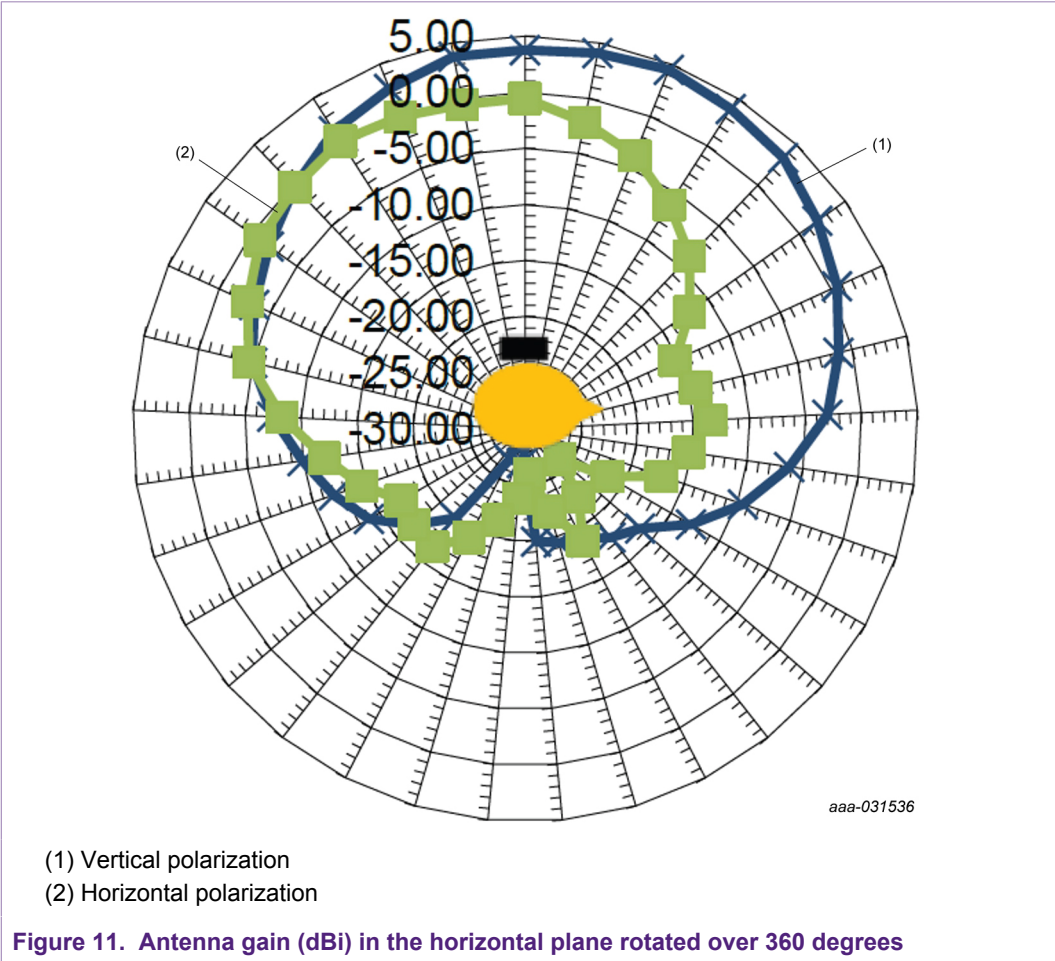


Table 3. Antenna gain (dBi) in the horizontal plane: maximum, minimum and average value over a rotating angle of 360 degrees in the horizontal plane

Gain (dBi)	Vertical polarization	Horizontal polarization
maximum	4.47	0.47
minimum	-33.93	-25.93
average	-8.25	-12.25

3.3 Conclusions on the antenna validation

As can be observed in this section, the antenna design targets are met:

- Return Loss  $|S_{11}| \leq -10$  dB from 2400 MHz to 2480 MHz

- Bandwidth  $\geq 300$  MHz
- Maximum gain  $\approx 0$  dBi for the vertical and the horizontal polarization
- The antenna supports the vertical and the horizontal polarization to a similar extent

The conductive parts inside the functional headphone results in additional antenna radiation at the other side of the head and drops in the radiation pattern.

One can therefore conclude that depending on the headphone design, incorporating this conductive plane antenna results in varying radiation patterns.

When considering a separation from the speaker and other conductive parts, the performance of the antenna reported here is safeguarded.

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